



# Cavities in Heat Transfer Models

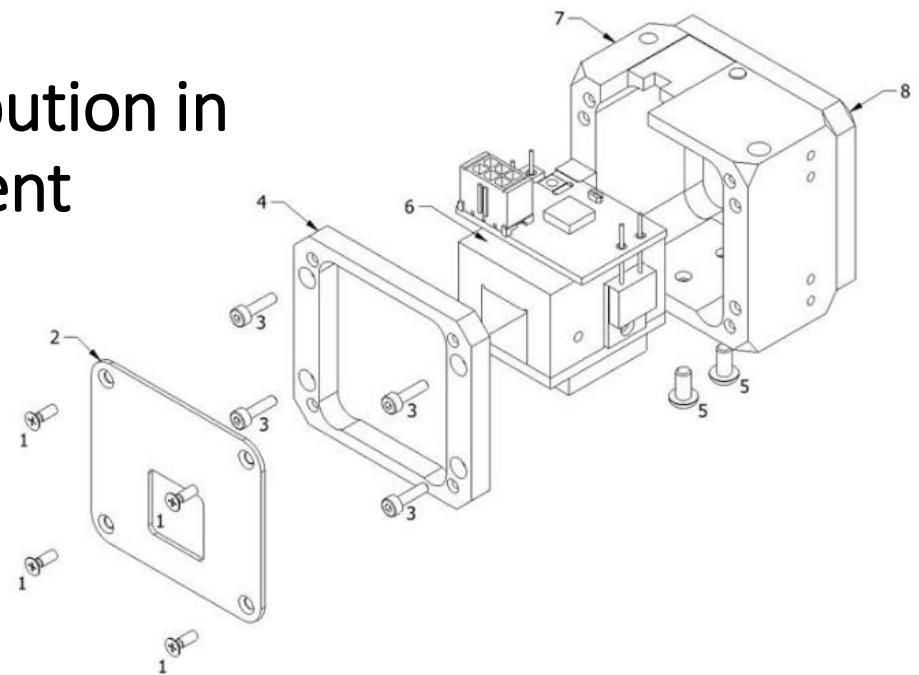
Tomas Tichy

# Crystal heating on specific temperature

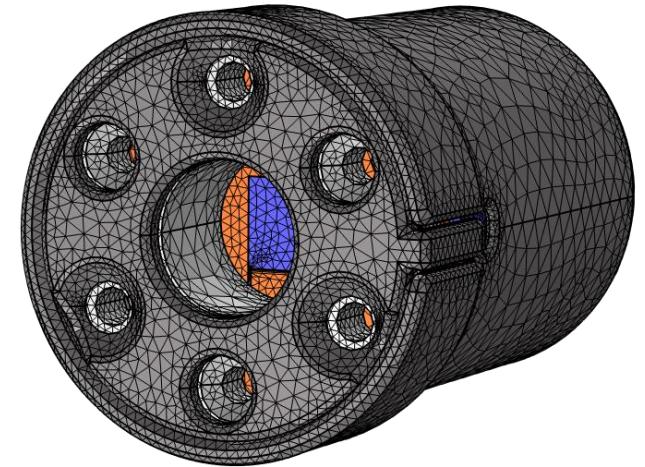
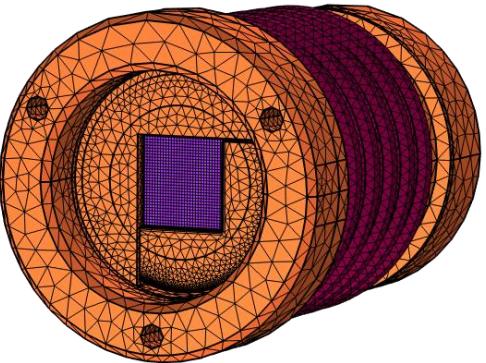
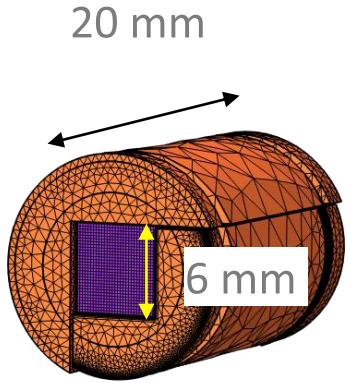
The LASER crystal must be heated on specific temperature, to provide optimal optical parameters



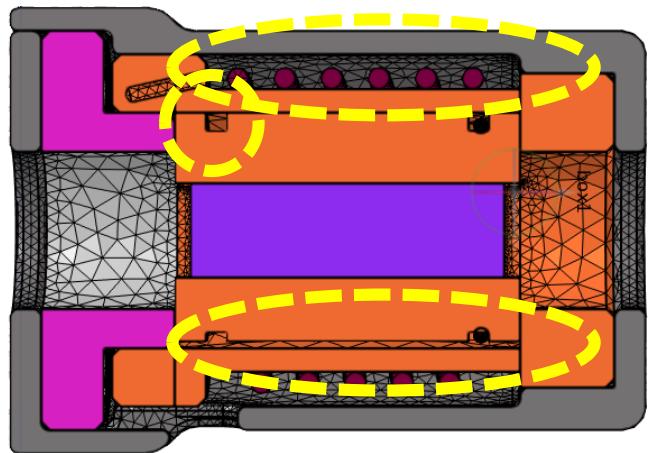
More important than exact temperature is the temperature distribution in crystal and T Gradient minimization



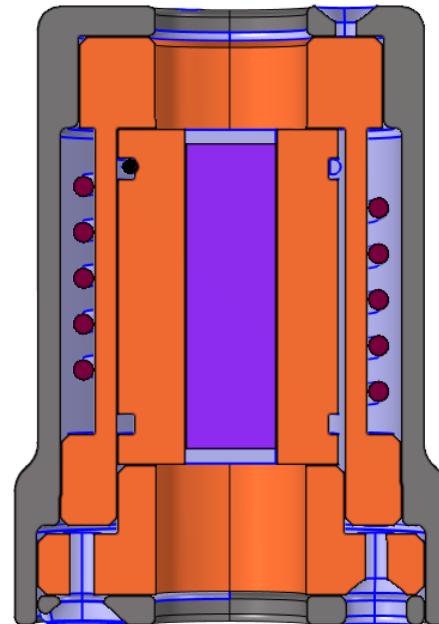
# Model of specific geometry for crystal oven



Many air cavities in the 3D geometry

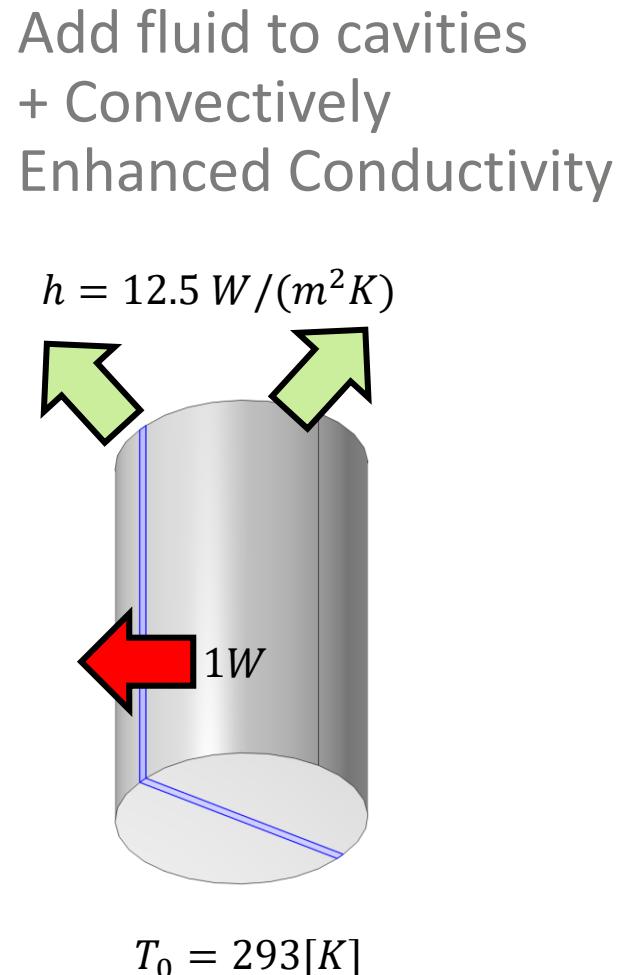
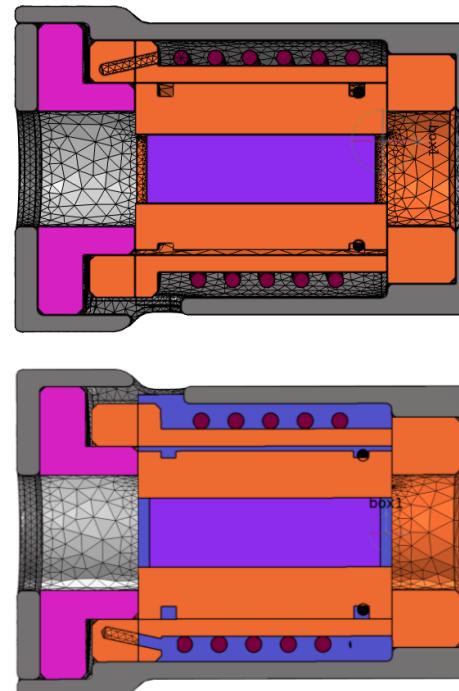
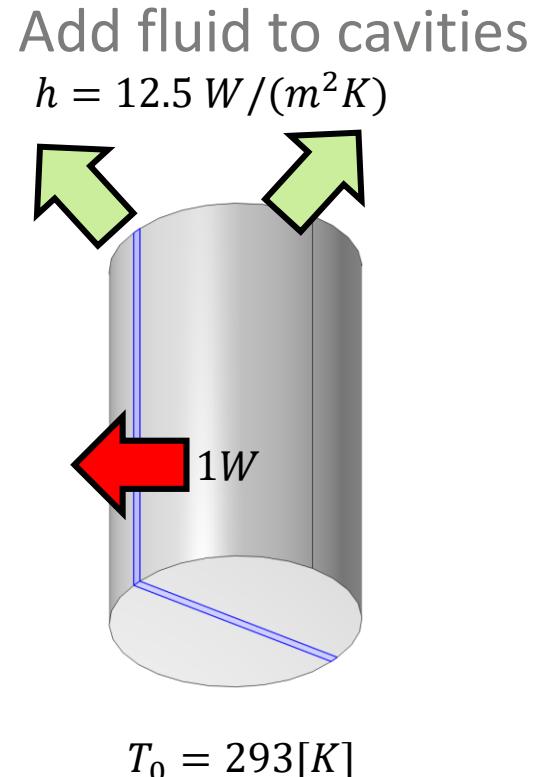
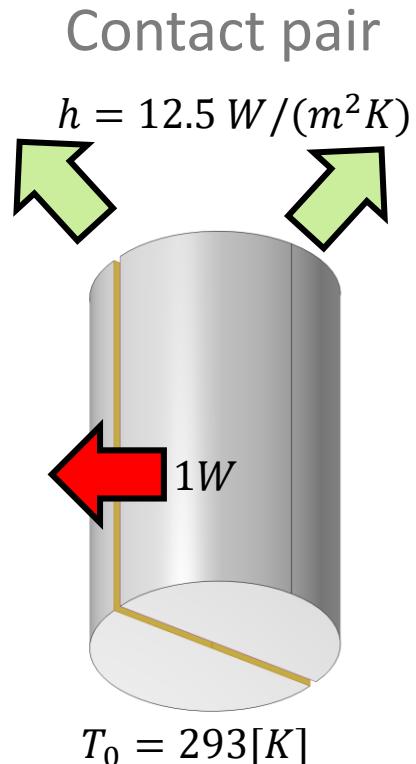


Default boundary condition:  
Thermal insulation



# Choices how to handle the cavities

Numerical vanishing of the cavities ?

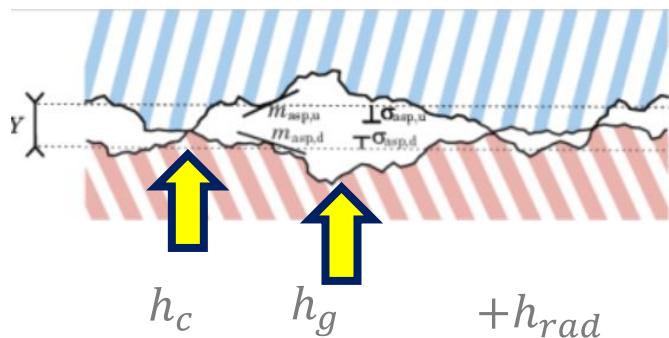


# Contact pair model

Thin structures → Thermal contact



Constriction Conductance with Interstitial Gas



$h_c$  - Constriction conductance =  $f(P, H_c, K_{contact})$

- Can be calculated by: Cooper-Mikic-Yovanovich Correlation (CMY)

Mikic Elastic Correlation

$h_g$  - Gap conductance =  $f(P, H_c, K_{contact})$

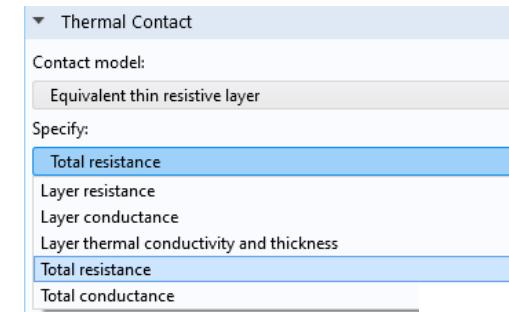
$$h_c = 1.25 \cdot K_{contact} \frac{m_{asp}}{\sigma_{asp}} \cdot \left( \frac{p}{H_c} \right)^{0.95}$$

$$h_g = \frac{k_g}{Y + M_g}$$

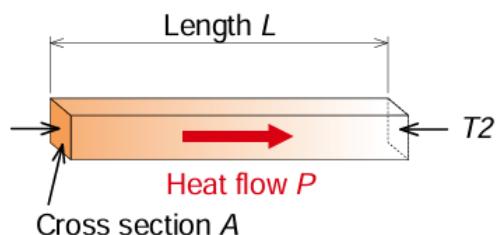
Coefficients calculated by  
Comsol (with user defined  
values) / user defined inputs

Equivalent Thin Resistive Layer

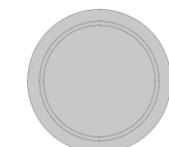
More possibilities how to set – see the [unit]



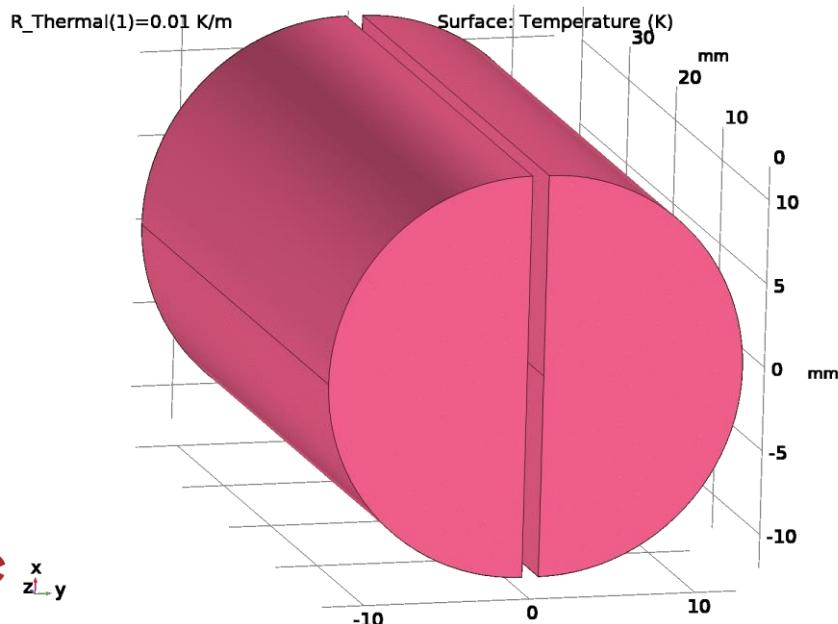
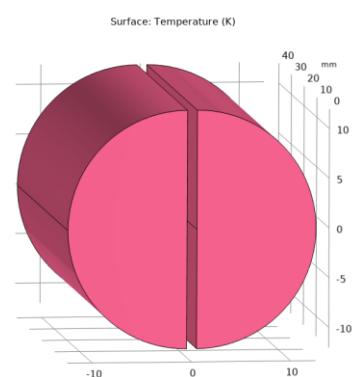
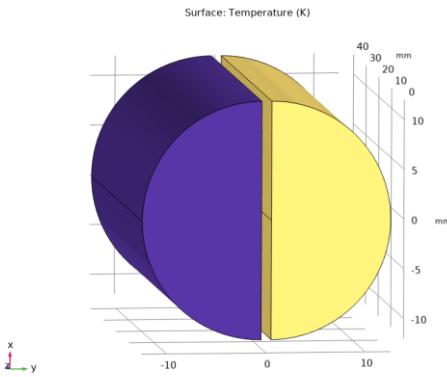
$$R_{th} = \frac{T_2 - T_1}{Q \cdot A} = \frac{1}{\lambda} \frac{L}{A} \left( \frac{K}{W} \right)$$



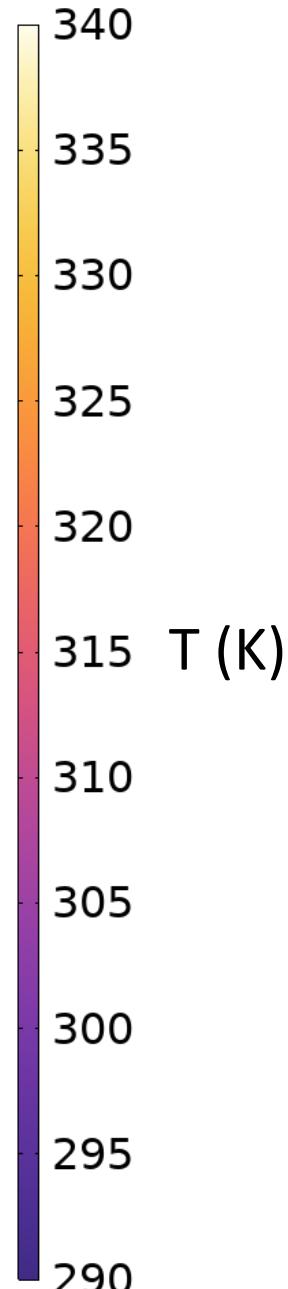
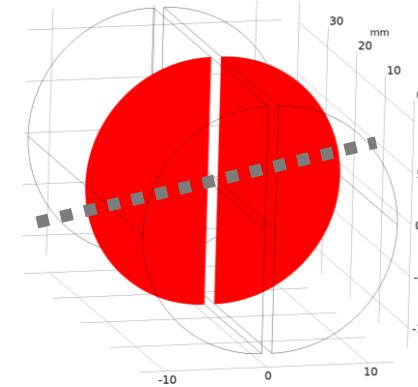
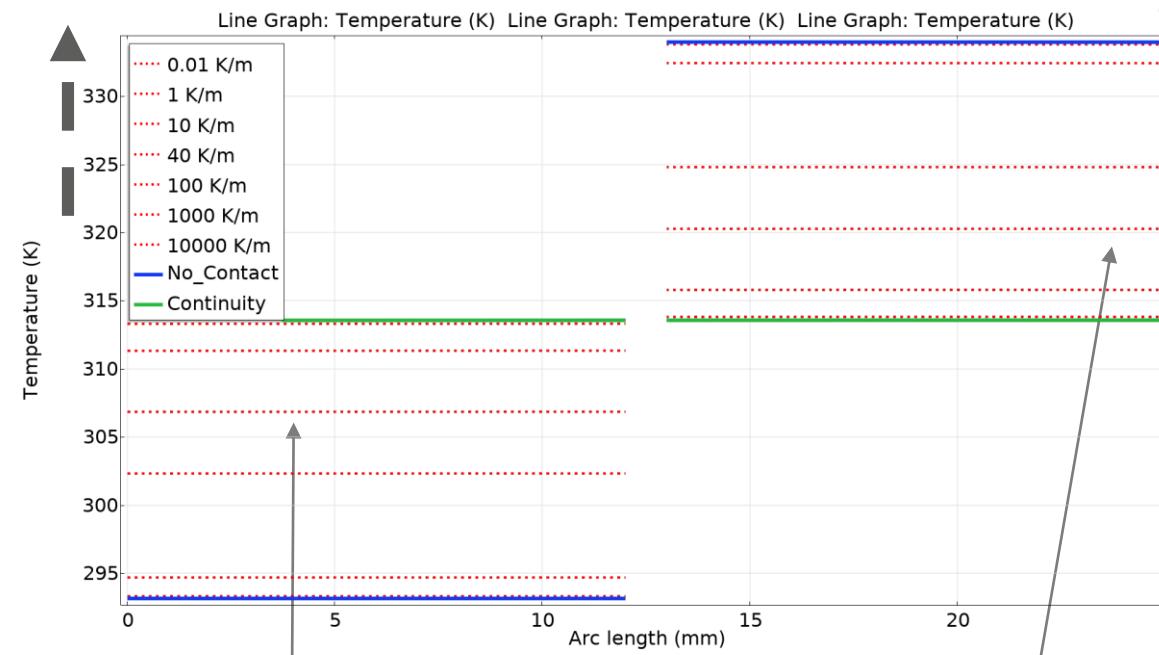
$$R_{th} = \frac{\ln(\frac{r_2}{r_1})}{k \cdot 2 \cdot \pi \cdot l} \left( \frac{K}{W \cdot m^2} \right)$$



# Contact pair model - results



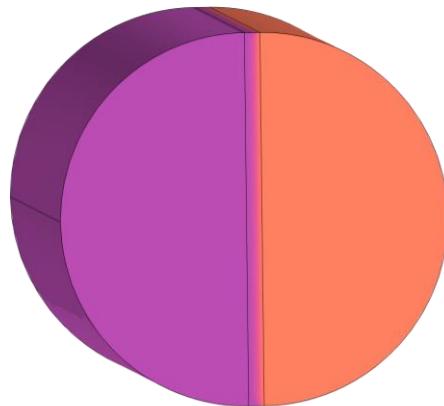
>R<sub>th</sub>



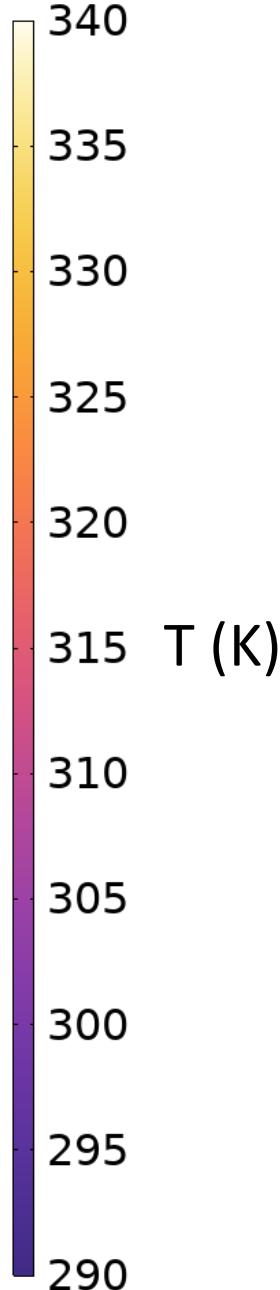
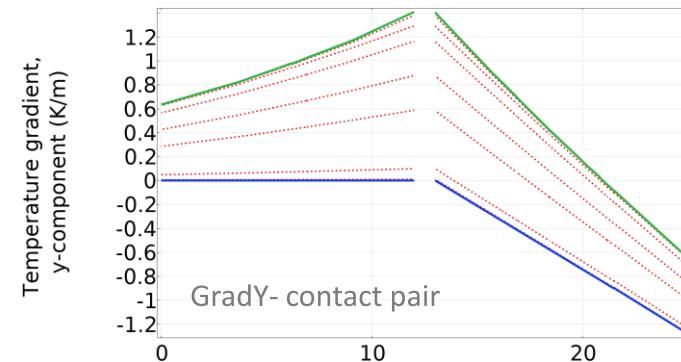
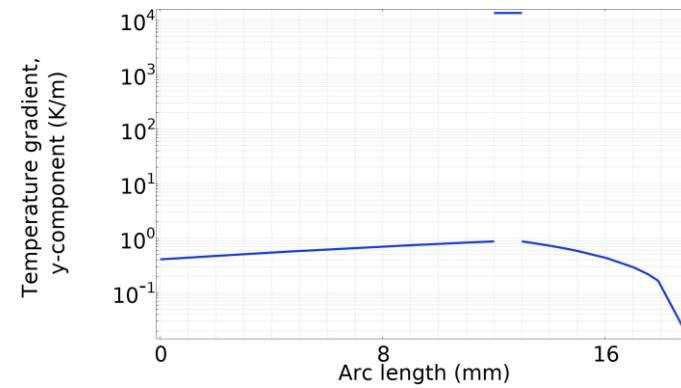
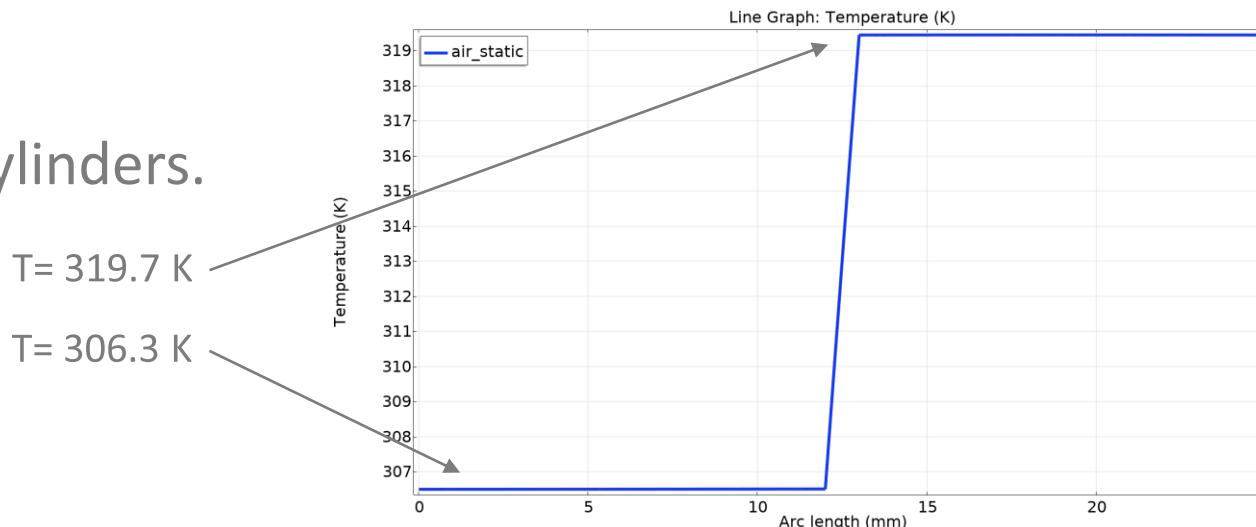
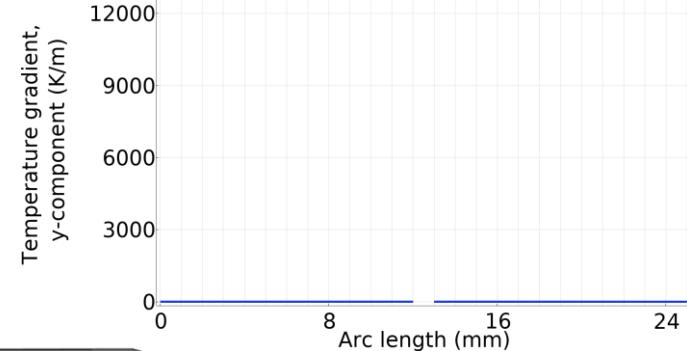
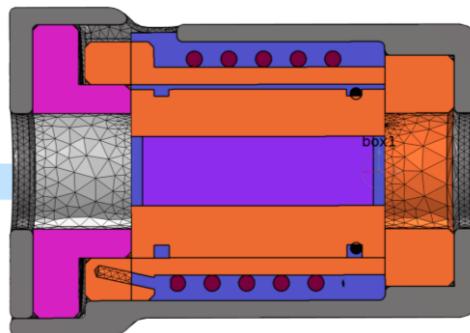
\*correct value of R<sub>th</sub> for our case is about 40 K/W.  
Than it becomes:  
T= 306.8 K  
T= 320.3 K

# Static fluid model

Added new domain between half-cylinders.  
Air material properties defined  
=simulation with static air

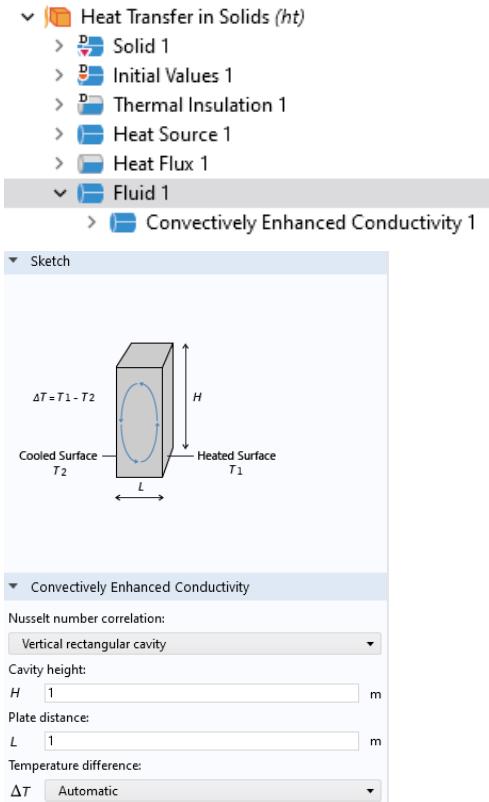


- ✓ Geometry 1
- ✓ LiveLink for SOLIDWORKS 2 (cad2)
- ✓ Cylinder 1 (cyl1)
- ✓ Difference 1 (dif1)
- ✓ Form Union (fin)

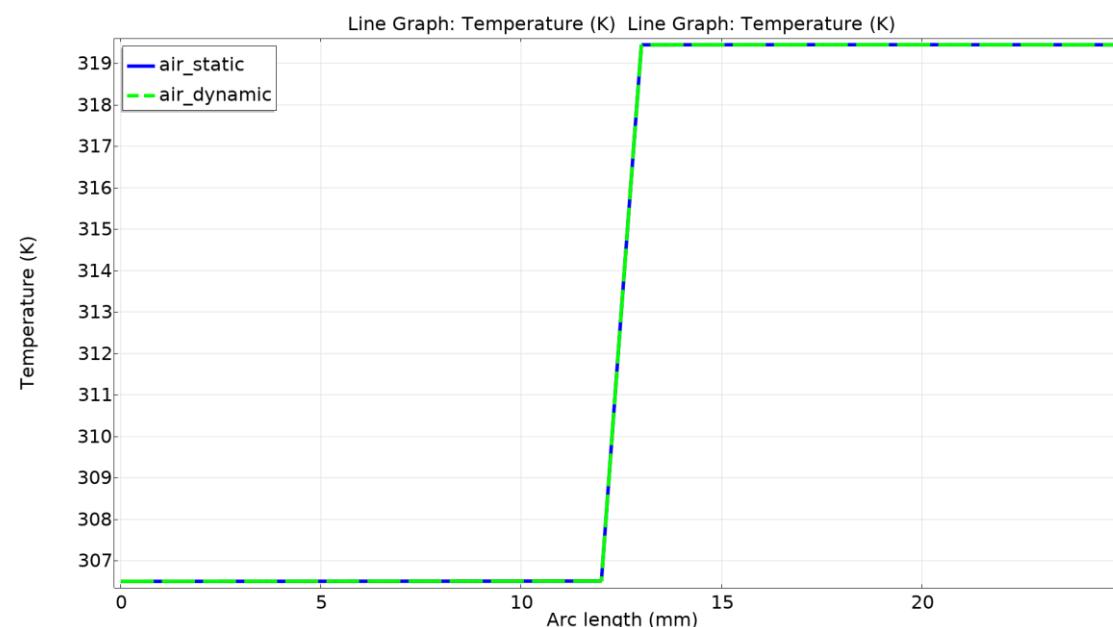


# Dynamic fluid model

Add FLUID volume condition to the ht physics. Then select:  
Convectively Enhanced Conductivity

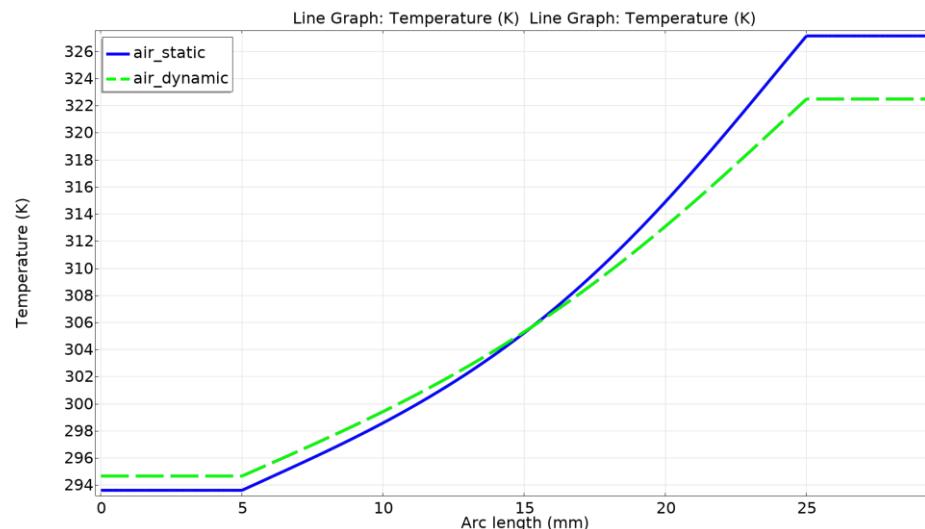
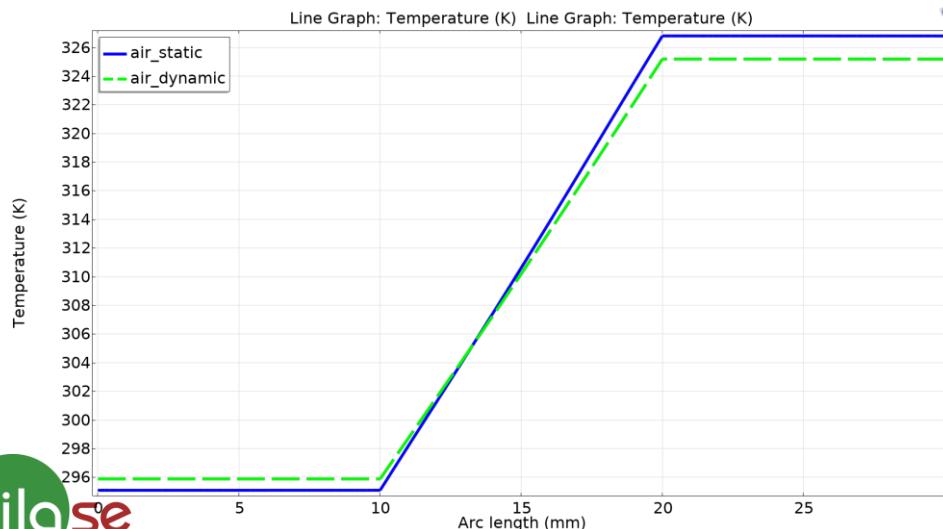
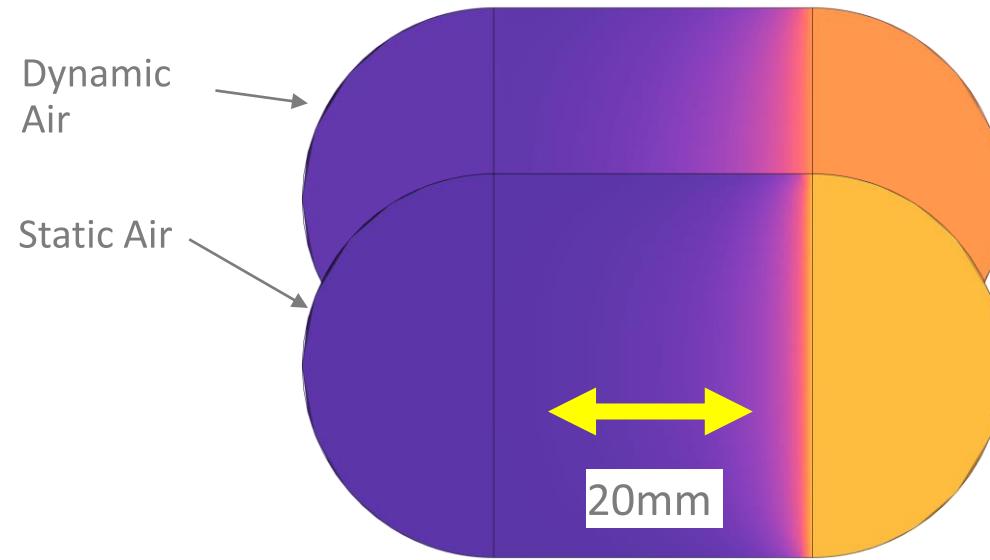
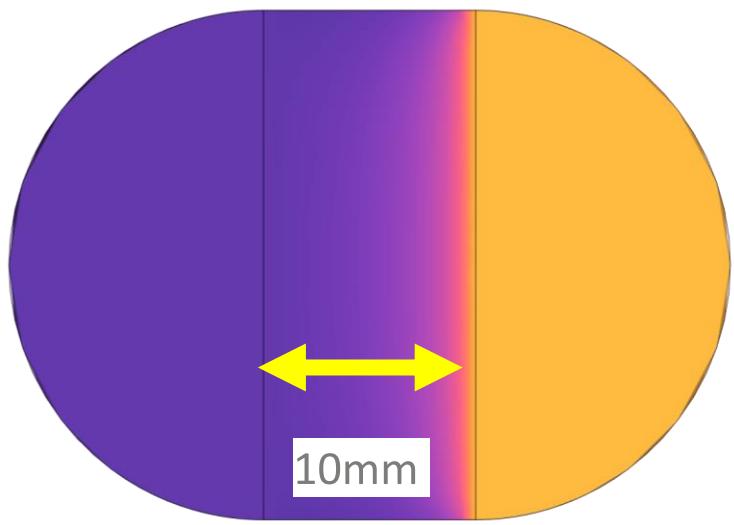


Uses Nusselt correlations for calculating heat transfer in cavity

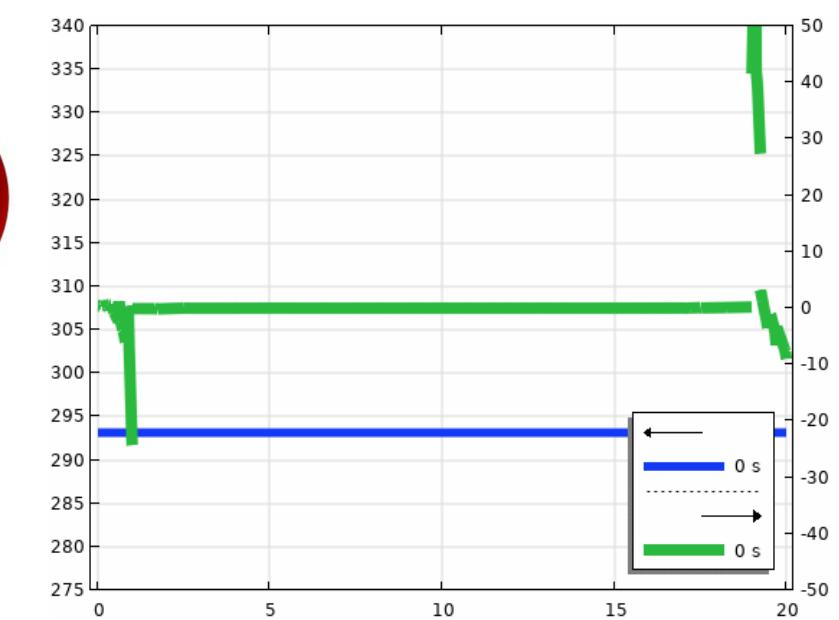
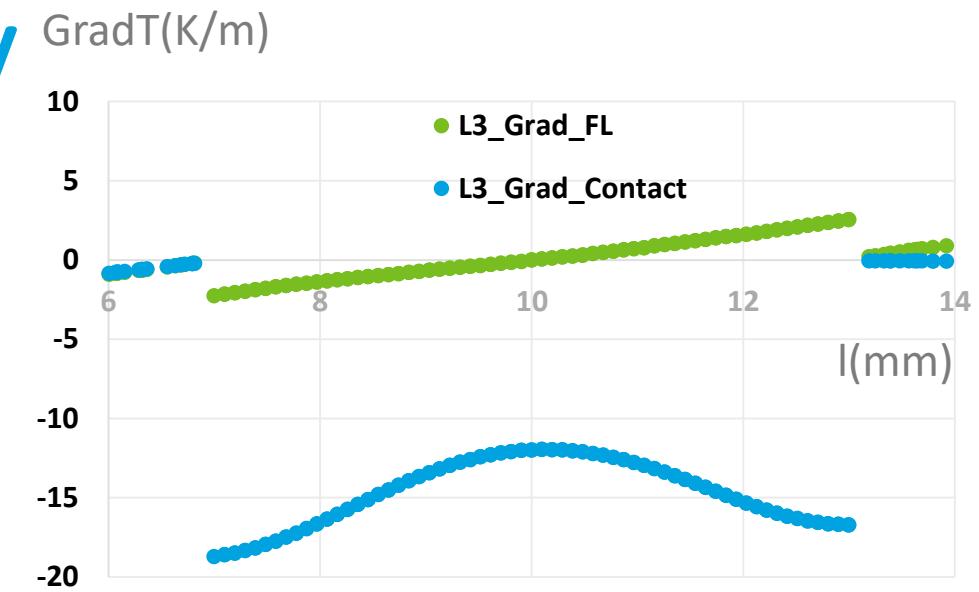
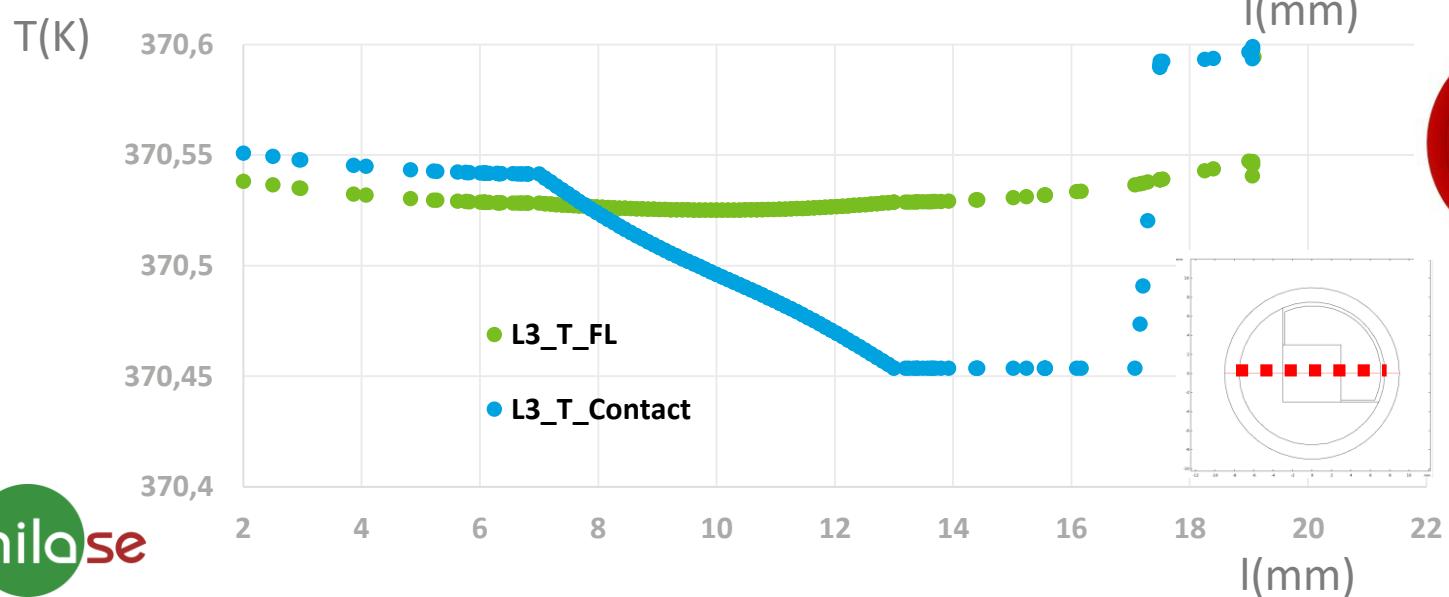
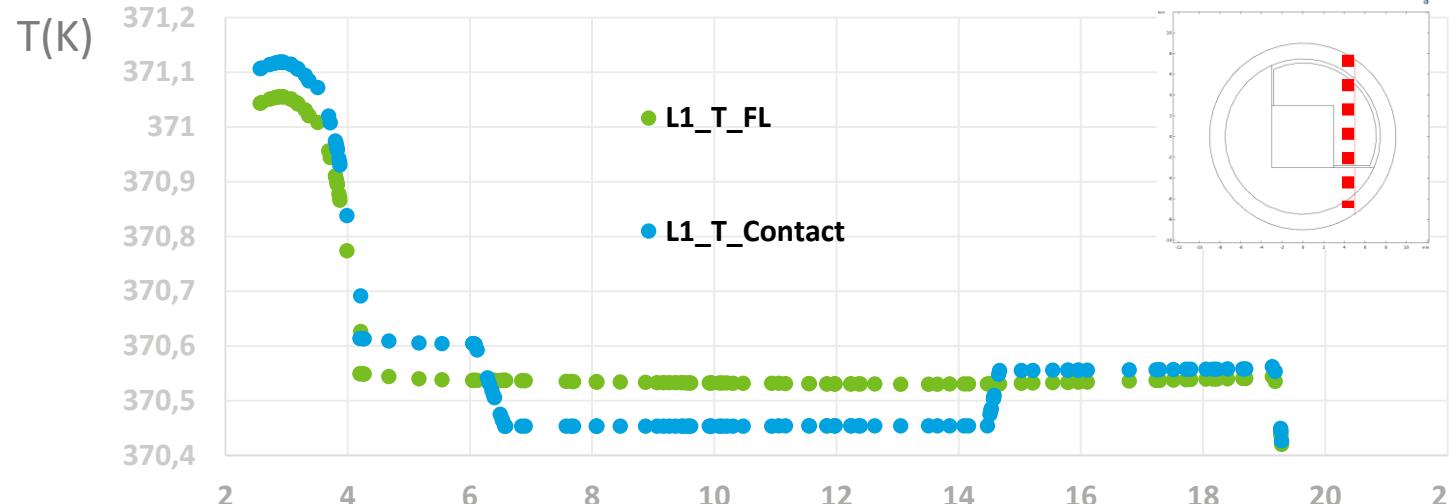


For current settings there is no significant difference between static and dynamic fluid model

# Static and Dynamic fluid comparation



# Cavities in (semi) real geometry



# Cavities in Heat Transfer Models

Cavities could be handled via:

- Equivalent thermal resistances
- Fluid infill of cavities



For real geometry *Convectively Enhanced Conductivity* was used mostly because „smooth“ gradient

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Other possible (future) ways:

Thermal resistances (thermal connection / lumped thermal port)

2-component model

Add radiation

Heat Transfer in Shells (Composite Thermal Barrier model from library)

References:

- [https://doc.comsol.com/5.5/doc/com.comsol.help.heat/he\\_at\\_ug\\_theory.07.66.html](https://doc.comsol.com/5.5/doc/com.comsol.help.heat/he_at_ug_theory.07.66.html)
- <https://www.omnicalculator.com/physics/thermal-resistance#how-to-use-the-thermal-resistance-calculator>
- <https://www.comsol.com/model/thin-film-resistance-31>
- [https://fscdn.rohm.com/en/products/databook/applinote/common/basics\\_of\\_thermal\\_resistance\\_and\\_heat\\_dissipation\\_an-e.pdf](https://fscdn.rohm.com/en/products/databook/applinote/common/basics_of_thermal_resistance_and_heat_dissipation_an-e.pdf)
- Základy sdílení tepla, Michail Michejev, Praha 1953, SNTL